



Steady State Behavior of Evaporation Unit in a Sugar Plant Using Markov Technique

KEYWORDS

Evaporating system; Steady state availability; Markov birth-death process, Transition diagram

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ABSTRACT This paper presents the steady state behavior of the evaporating system in a sugar plant. The sugar plant comprises of various systems including feeding, crushing, evaporating, refining, crystallization etc. One of the most important functionalities of a sugar plant, on which quality of sugar depends, is the evaporating system, where it is ensured that the desired viscosity is obtained. The evaporating system consists of two subsystems arranged in series with three states; reduced capacity, good and failure. The mathematical modeling is carried out on the basis of Markov birth-death process using a probabilistic approach. An expression for steady state availability is also developed. The findings of this paper have been discussed with the concerned plant personnel and found to be highly beneficial for enhancing the performance level of the plant concerned.

1. INTRODUCTION

In the process industries, maintenance is considered as an integral part of the production process. It is done by maintaining resources and by ensuring high availability level. For increasing the productivity and availability of equipment, subsystems and systems in operation must be maintained at the highest order. To achieve high production goals, the systems should remain operative for maximum possible time duration. But practically these systems are subject to random failures due to the poor design, wrong manufacturing techniques, lack of operative skills, poor maintenance, overload, delay in starting maintenance, human errors, etc. These causes lead to non-availability of an industrial system resulting into improper utilization of resources. So, to achieve high production targets, there should be long-run system availability.

2. SYSTEM DESCRIPTION

Evaporation unit consists of two subsystems in series configuration with the following description: Subsystem D_i ($i = 1$ to 4): It consists of four evaporation units connected in parallel. The failure of any one reduces the capacity of the system and, hence loss in production. Complete failure occurs when more than two unit fail at a time. Subsystem E_j ($j = 1$ to 3): It consists of three pans units connected in parallel. Complete failure occurs when more than one unit fail at a time.

3. ASSUMPTIONS

The assumptions used in the probabilistic model are as follows:

1. Failure/repair rates are constant over time and statistically independent.
2. A repaired unit is as good as new and performance wise for a specified duration.
3. Sufficient repair facilities are provided, i.e., no waiting time to start the repairs.
4. Standby units (if any) are of the same nature and capacity as the active units.
5. System failure/repair follows exponential distribution.
6. Service includes repair and replacement.
7. System may work at a reduced capacity/efficiency.
8. There is no simultaneous failure among the system.

4. NOTATIONS

The following notations are associated with the evaporation unit:

D_i, E_j : Represent good working states of respective evaporator and pans

d, e : Represent failed states of respective evaporator and pans

Φ_1, Φ_2 : $r \Phi_1, \Phi_2$: respective mean constant failure rates D_i, E_j

λ_1, λ_2 : respective mean constant repair rates of d_i, e_j

d/dt : represents derivative w.r.t 't'

$P_i(t)$: state probability that the system is in i th state at time t .

This system consists of 12 states as:

State 0- Full capacity working with no standby

States 1,2,3,4,5- Reduced capacity working

States 6,7,8,9,10 – System in failed state due to complete failure of one or other unit of the system.

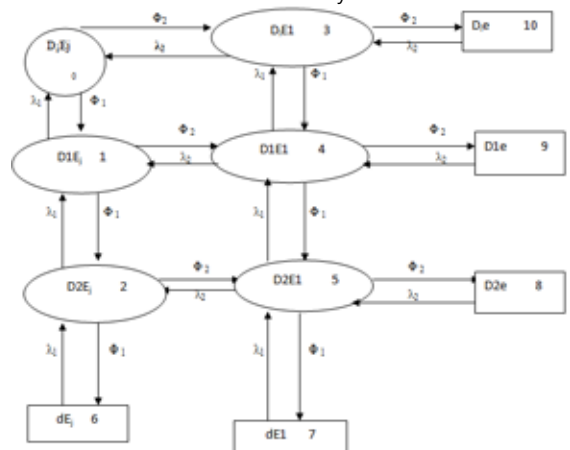


Figure 1 Transition Diagram of Evaporation System

5. MATHEMATICAL MODELING

The differential equations associated with the transition diagram of the evaporation system are as follows:

$$P0(t) (d/dt + \Phi2 + \Phi1) = P1(t) \lambda1 + P3(t) \lambda2 \dots\dots 1$$

$$P1(t) (d/dt + \Phi1 + \Phi2 + \lambda1) = P4(t) \lambda2 + P2(t) \lambda1 + P0(t) \Phi1 \dots\dots\dots 2$$

$$P2(t) (d/dt + \Phi1 + \Phi2 + \lambda1) = P6(t) \lambda1 + P1(t) \Phi1 + P5(t) \lambda2 \dots\dots\dots 3$$

$$P3(t) (d/dt + \lambda2 + \Phi2 + \Phi1) = P0(t) \Phi2 + P10(t) \lambda2 + P4(t) \lambda1 \dots\dots\dots 4$$

$$P4(t) (d/dt + \lambda1 + \lambda2 + \Phi2 + \Phi1) = P1(t) \Phi2 + P5(t) \lambda1 + P9(t) \lambda2 + P3(t) \Phi1 \dots\dots\dots 5$$

$$P5(t) (d/dt + \lambda1 + \lambda2 + \Phi2 + \Phi1) = P4(t) \Phi1 + P2(t) \Phi2 + P8(t) \lambda2 + P7(t) \lambda1 \dots\dots\dots 6$$

$$P6(t) (d/dt + \lambda1) = P2(t) \Phi1 \dots\dots\dots 7$$

$$7(t) (d/dt + \lambda1) = P5(t) \Phi1 \dots\dots\dots 8$$

$$P8(t) (d/dt + \lambda2) = P5(t) \Phi2 \dots\dots\dots 9$$

$$P9(t) (d/dt + \lambda2) = P4(t) \Phi2 \dots\dots\dots 10$$

$$P10(t) (d/dt + \lambda2) = P3(t) \Phi2 \dots\dots\dots 11$$

6. STEADY STATE AVAILABILITY

The steady state behavior of the system can be analyzed by setting $t \rightarrow \infty$ and $d/dt \rightarrow 0$. The limiting probabilities from equations (1) – (11) are:

On solving these equations recursively, we get:

$$P1 = P0J36$$

$$P2 = P0J37$$

$$P3 = P0J40$$

$$P4 = P0J39$$

$$P5 = P0J38$$

$$P6 = P0J37K1$$

$$P7 = P0J38K1$$

$$P8 = P0J38K2$$

$$P9 = P0J39K2$$

$$P10 = P0J40K2$$

Where

$$K2 = \phi1 / \lambda1$$

$$K1 = \phi2 / \lambda2$$

$$J1 = \lambda1 (\phi1 + \phi2 + \lambda1)$$

$$J2 = \lambda2 (\phi1 + \lambda2)$$

$$J3 = (\phi1\lambda1) + (\phi2\lambda2)$$

$$J4 = \phi2 + \lambda1$$

$$J5 = (\lambda1\lambda1\phi1) + (J1J4)$$

$$J6 = J3\phi1$$

$$J7 = J2\phi1$$

$$J8 = J1 \lambda2$$

$$J9 = (J5\lambda1) + (J5\lambda2) + (J8\phi2)$$

$$J10 = J6\phi2$$

$$J11 = J7\phi2$$

$$J12 = J5\phi1$$

$$J13 = \phi1 + \lambda2$$

$$J14 = (J11\lambda1) / J13$$

$$J15 = (J11\phi2) / J13$$

$$J16 = (J10 - J15) / J9$$

$$J17 = (J12 - J14) / J9$$

$$J18 = (J16\lambda1) + J16\lambda2$$

$$J19 = (J17\lambda1) + (J17\lambda2) - \phi1$$

$$J20 = J18 - (J16J19)$$

$$J21 = J17\phi2$$

$$J22 = J21\phi1$$

$$J23 = J4J20$$

$$J24 = (J19J4) - (J21\lambda2)$$

$$J25 = (J22\lambda2) + (J24\phi1)$$

$$J26 = J23\lambda2$$

$$J27 = J4J24$$

$$J28 = (\phi1 + \phi2 + \lambda1) (J27J19)$$

$$J29 = \lambda1J25J19$$

$$J30 = \lambda1J26J19$$

$$J31 = \phi2\lambda2J27$$

$$J32 = J18\lambda2J27$$

$$J33 = \phi1J19J27$$

$$J34 = J28 - J29$$

$$J35 = J33 - J32 - J30$$

$$J36 = [(J35J27) - (J26J31)] / [(J34J27) + (J25J31)]$$

$$J37 = [(J36J25) - (J26)] / (J27)$$

$$J38 = [(J37J21) + (J21)] / (J19)$$

$$J39 = (J38 - J16) / (J17)$$

$$J40 = [(J6) - (J38J8) + (J37J5)] / (J7)$$

$$P0 + P1 + P2 + P3 + P4 + P5 + P6 + P7 + P8 + P9 + P10 = 1$$

$$P0 + P0J36 + P0J37 + P0J40 + P0J39 + P0J38 + P0J37K1 + P0J38K1 + P0J38K2 + P0J39K2 + P0J40K2 = 1$$

$$P0 [1 + J36 + J37 + J40 + J39 + J38 + J37K1 + J38K1 + J38K2 + J39K2 + J40K2] = 1$$

$$P0=1/[1+ J36+ J37+ J40+ J39 + J38 + J37K1 + J38 K1 + J38K2 + J39K2 + J40 K2]$$

Now, the steady state availability (Av) of evaporation system is given by summation of all the full working and reduced capacity states probabilities.

$$Av = P0 + P1+P2+P3+P4+P5$$

7. BEHAVIOR ANALYSIS OF EVAPORATION SYSTEM

By critically examining the process of evaporation system and taking the relevant values of the failure and repair rates of each subsystem, the effect of these parameters on the system availability has been shown in Tables.

Table 1 Availability matrices for 'evaporator' subsystem of evaporation system Constant values are: $\Phi1=0.010$, $\lambda1=0.02$

AV →

$\lambda2$ / $\Phi2$	0.01	0.015	0.020	0.025	0.030
0.003	.716699	.784015	.823309	.848835	.866750
0.004	.658334	.737109	.784015	.815138	.837297
0.005	.609483	.695498	.748301	.784015	.809781
0.006	.567381	.658334	.715699	.755181	.784015
0.007	.530720	.624941	.685819	.728393	.759839

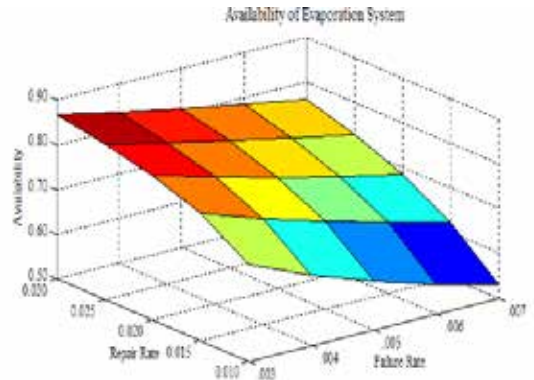


Figure 3 Effect of failure and repair rate of 'cooking pan' subsystem on system availability

8. RESULTS AND DISCUSSION

It is observed that for some known values of failure / repair rates of evaporator and cooking, as the failure rate of evaporator increases from 0.003 (once in 333.3 hrs) to 0.007 (once in 142.85 hrs), the system availability decreases drastically by 18.6%. Similarly as repair rate of evaporator increases from 0.010 (once in 100 hrs) to 0.030 (once in 33.3 hrs), the system availability increases considerably by 15%.

Also, as the failure rate of cooking pan increases from 0.005 (once in 200 hrs) to 0.009 (once in 111.11 hrs), the system availability decreases marginally by 11.1%. Similarly as repair rate of cooking pan increases from 0.02 (once in 50 hrs) to 0.06 (once in 16.6 hrs), the system availability increases considerably 12.5%.

9. CONCLUSIONS

It can thus be concluded that the steady state behavior of evaporation system can be analyzed with the help of availability model developed. The behavior analysis has also been explained by means of availability Tables (1, 2). These availability tables show the effect of failure and repair rates of various subsystems on the steady state availability of evaporation system. Probabilistic models for various subsystems of a sugar plant have been developed and analyzed in real environment. The steady state availability expressions have been derived. The inter-relationships among various working units in the operating environment have been developed. Availability matrices have been developed which help in deciding availability and performance level. The effect of each unit behavior on the system performance has also been analyzed through availability matrices and availability plots. Desired level of performance has been established and the practical values of states of nature and courses of action have been determined.

Figure 2 Effect of failure and repair rate of 'evaporator' subsystem on system availability

Table 2 Availability matrices for 'cooking pan' subsystem of evaporation system

AV →

$\lambda1$ / $\Phi1$	0.02	0.03	0.04	0.05	0.06
0.005	.758186	.816091	.858424	.869251	.883641
0.006	.727152	.791877	.828762	.852590	.869251
0.007	.698601	.769059	.809900	.836555	.855322
0.008	.672208	.747518	.791877	.821113	.841833
0.009	.647736	.727152	.774639	.806230	.828762

Constant values are: $\Phi2=0.001$, $\lambda2=0.05$

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