



# Analytical Investigation of Motor-Vehicle Kinematics Parametres at Acceleration During Rectilinear Motion

## KEYWORDS

transitional operation modes, velocity and acceleration of motor-vehicle, rectilinear motion, external and partial velocity characteristics of internal combustion engine

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**ABSTRACT** A procedure for analytical investigation of the velocity indices (velocity and acceleration) at motor-vehicle acceleration during rectilinear motion is hold out in this study. The results obtained by the numerical experiment are presented graphically, and their adequacy with the natural experiment is demonstrated.

## Introduction

The transitional (unsettled) operation modes of motor-vehicles are a significant part of motion time in urban and out-of-town conditions during maneuvers requiring gear shifting. The main indices of the transitional operation modes of motor-vehicle are the changes of velocity and acceleration.

The goal of this study is the formation of a procedure for analytical determination of motor-vehicle kinematics parameters at rectilinear motion during the start from out-of-motion position up to the reach of settled operation mode at a certain gear.

## Mathematical Modeling

A priority of analytical determination of motor-vehicle basic velocity properties such as velocity and acceleration is that the mathematical dependences give a possibility for numerical examinations of a wide spectrum of motor-vehicles.

The modeling of transitional operation modes of a motor-vehicle during engine work at external velocity characteristic is not precise, and therefore it is necessary the transitions upon the partial characteristics at incomplete fuel-feeding to be read. In this connection the engine is described with a characteristic representing the moment in a dependence of two parameters,  $n$  and  $\gamma$ , the frequency of rotation of engine crankshaft and the position of fuel-feeding pedal, respectively. This dependence is obtained as a result of the approximation of the experimental data represented in [1].

(1)

$$M_d = f(n, \gamma)$$

The procedure for the carrying out of numerical investigations for the obtaining of engine moment change at transitional operation modes is described in details in [2].

The motor-vehicle rectilinear motion is described using the equation of motor-vehicle during clear rolling of wheels got in article [3].

$$\ddot{x} = \frac{1}{\left(m + \frac{I_1 + I_2}{r^2}\right)} \cdot \left[ \frac{M_d}{r} - m \cdot g \cdot (f \cdot \cos \alpha \pm \sin \alpha) - w \cdot \dot{x}^2 \right] \quad (2)$$

where  $m$  is motor-vehicle mass;  $I_1$  and  $I_2$  are the mass moments of inertia of the drive and driven gears, respectively;  $M_d$  is the motor moment deduced towards the axes of wheels;  $g$  is acceleration of gravity;  $f$  is a of rolling resistance coefficient;  $w$  is the factor of streamlining;  $\alpha$  is the angle of road longitudinal slope.

The motion of motor-vehicle with clutch slippery at gear change is described with integral-differential systems of equations, represented in details in [2].

$$\begin{aligned} I_d \cdot \ddot{\varphi}_d &= M_i(\dot{\varphi}_d) - M_M(\dot{\varphi}_d) - M_r(t) \\ I_{a_j} \cdot \ddot{\varphi}_c &= M_r(t) - M_s(\dot{\varphi}_c) \\ A_b &= \int_0^t M_r(t) \cdot (\dot{\varphi}_d - \dot{\varphi}_c) \cdot dt \end{aligned} \quad (3)$$

where  $\dot{\varphi}_d$  is the angular velocity of crankshaft;  $\dot{\varphi}_c$  is the angular velocity of clutch shaft;  $I_d$  is the mass inertia moment of the motor-vehicle engine reduced to the crankshaft;  $I_{a_j}$  is the mass inertia moment of the motor-vehicle of the  $j^{\text{th}}$  gear reduced to the clutch shaft;  $M_i(\dot{\varphi}_d)$  is an indicator torque of the engine;  $M_M(\dot{\varphi}_d)$  is a moment of mechanical losses in the engine;  $M_s(\dot{\varphi}_c)$  is the resistance moment caused by the external load supplied upon the engine shaft;  $M_r(t) = \psi \cdot t$  is the friction moment of the clutch;  $\psi$  is a coefficient reading the speed of increase of clutch friction moment;  $A_b$  is the slippery work of the clutch.

The developed mathematical model is realized in a medium of imitation-mathematical modeling of dynamic systems Simulink of the programme product Matlab. The model includes the following basic stages:

I – engine operation in a regime of idle running (section 1 in Fig. 1);

II – acceleration of motor-vehicle with slippery clutch and put in 1<sup>st</sup> gear up to the equalization of the angular velocities of crankshaft and clutch shaft (section 2 in Fig. 1);

III – acceleration of motor-vehicle at put in 1st gear at equalized angular velocities of crankshaft and clutch shaft

(section 3 in Fig. 1);

IV – shifting II<sup>nd</sup> gear at clutch release (section 4 in Fig. 1);

V – acceleration of motor-vehicle with slippery clutch and put in II<sup>nd</sup> gear (section 5 in Fig. 1);

### Results

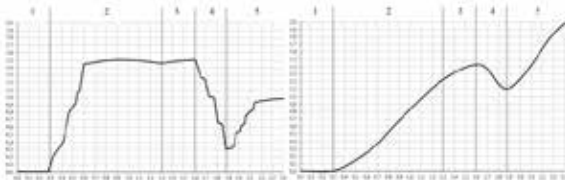
The change of the engine angular velocity in the course of time at operation in a regime of idle running to the reach of magnitude  $\dot{\varphi}_{d_0}$  at zero angular velocity of clutch is determined during the first stage. The first equation of system (3) at  $M_r(t) = 0$  is solved.

During the second stage the system (3) is solved up to the equalization of the angular velocities of crankshaft and clutch shaft  $\dot{\varphi}_d = \dot{\varphi}_c$ .

During the third stage is solved the first equation of system (3) at  $M_r(t) = M_s(\dot{\varphi}_d)$ , where  $M_s(\dot{\varphi}_d)$  is the resistance moment caused by the external load supplied upon the engine shaft.

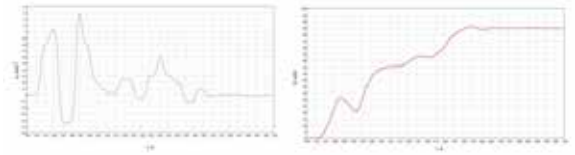
For the fourth stage the first two equations of the system (30) are solved at  $M_r(t) = 0$ , while the system (3) at put in II<sup>nd</sup> gear is solved during the fifth stage.

The changes of the acceleration and the velocity of engine mass centre during the start from out-of-motion position up to the reach of a velocity chosen by the driver at put in II<sup>nd</sup> gear are represented in Fig. 1.



**Fig. 1. Time dependence of the acceleration and the velocity of engine mass centre**

The adequacy of the model is proved by the experimental data obtained for a motor-vehicle with close mass and technical characteristics placed at our disposal by Assoc. Prof. Nedelcho Ivanov, Ph D, who is a university teacher in Technical University in Varna (Fig. 2 ). The numerical experiments carried out are for a period corresponding to the period of the natural experiments up to 400 s.



**Fig. 2. Time dependence of the acceleration and of the velocity of engine mass centre**

### Conclusion

The experimental results show the practical applicability of the mechano-mathematical model for motor-vehicle acceleration during the start from out-of-motion position up to the reach of a settled operation at a certain gear. The procedure suggested is useful for the determination of a velocity and acceleration of a motor-vehicle during the drawing up of an auto-technical expertise, when the precision of the determination is of special meaning.

### REFERENCE

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